

Optimal Observer Synthesis for Microgrids With Adaptive Send-on-Delta Sampling Over IoT Communication Networks

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Abstract—State estimation is one of the main challenges in the microgrids, due to the complexity of the system dynamics and the limitations of the communication network. In this regard, a novel real-time event-based optimal state estimator is introduced in this article, which uses the proposed adaptive send-on-delta (SoD) nonuniform sampling method over wireless sensors networks. The proposed estimator requires low communication bandwidth and incurs lower computational resource cost. The threshold for the SoD sampler is made adaptive based on the average communication link delay, which is computed in a distributed form using the event-based average consensus protocol. The SoD nonuniform signal sampling approach reduces the traffic over the wireless communication network due to the events transmitted only when there is a level crossing in the measurements. The state estimator structure is extended on top of the traditional Kalman filter with the additional stages for the fusion of the received events. The error correction stage is further improved by optimal reconstruction of the signals using projection onto convex sets algorithm. Finally, an Internet of things (IoT) experimental platform based on LoRaWAN and IEEE 802.11 (WiFi) protocols are developed to analyze the performance of the state estimator for the IEEE 5 Bus case study microgrid.

Index Terms—Event-based state estimation, Internet of Things (IoT), LoRaWAN, microgrid, POCS, real-time simulation, send-on-delta kalman filter, thingsboard.

I. INTRODUCTION

MICROGRIDS are small scale power systems that have been proposed for the optimal integration of renewable energy resources (RESs). However, having the smaller scale has decreased the inertia required for the stability of its operation, similar to any other fast dynamic system. Low inertia means that the system is prone to instabilities driven by disturbances

more, and therefore robust controllers should be designed to stabilize its long-term operation [1], [2]. The main element of the robust controllers is the adaptation to the current state of the system, as a high number of the robust control techniques are based on state feedback [3], [4]. To address this requirement, observers are used for monitoring the state of the system because the state variables of a complex system are not available for direct measurement through the system outputs. Furthermore, due to the measurement noise, process noise, and the communication restrictions, continuous noise-free measurements are not available at the observers, which mandates the usage of estimation strategies in them [5], [6]. Additionally, the fast dynamic of the microgrid necessitates that this estimation takes place in real-time [7].

Two main approaches are proposed in the literature of state estimators, i.e., centralized and distributed strategies. These approaches have their own advantages, which suits them for the specific user application. Distributed state estimation strategies are usually used when the dynamic system has a large scale and the computation resource cost of a centralized option makes the solution expensive and infeasible [8]. Despite distributed approaches solve the single failure point issue, they mandate the use of more measurement nodes, which is not suitable for medium sized microgrids [9], [10].

Contrary to distributed approaches, in centralized state estimators, the main assumption is to have a single node for the whole state estimation task. Therefore, computationally powerful measurement nodes are not needed as they have to only collect the data and transmit it [11], [12]. The data transmission rate of the sensors significantly affects the performance of the estimator, the energy consumption of battery-based devices, and the network traffic [13]. Most of the classic estimation theories have assumed that the signals are either continuous or sampled periodically with a constant period. However, the current communication technology trend is to use Internet of things (IoT) communication networks, which has constraints in the communication speed and its availability [7]. These limitations mandates the use of modern techniques and theories for the state estimation to work based on nonuniform event-based data from the measurements in a microgrid. For example, authors in [14] used nonsynchronized measurements from the smart meters, or the authors in [15] have used continuous measurements to find

Manuscript received June 11, 2020; revised August 13, 2020; accepted October 20, 2020. Date of publication November 4, 2020; date of current version July 19, 2021. (Corresponding author: Seyed Amir Alavi.)

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Digital Object Identifier 10.1109/TIE.2020.3034853

an accurate multilevel estimation strategy. Other studies such as [16]–[18], have tried to reduce the state space set and have used classic estimators, which are not optimal in resource utilization. A data-driven approach is also proposed in [19], which is able to work under uncertainties, with the cost of offline training. Several other works have been reported in the literature to address the sampling issue in IoT networks from the rate adaptiveness perspective. In those works, instead of having the samples at unevenly distributed discrete instants, the periodic sampling rate is adaptively adjusted. In [20], AdaM algorithm is proposed which integrates a filtering unit along with the sampler. This approach increases the computing burden on the device, as it has to solve an optimization problem in real-time. In [21], a differential privacy-based sampling method is proposed, which hides the data correlation from the malicious attacker, with the cost of data encoding/decoding at both the transmitter and receiver ends. A co-design method is proposed in [22], that considers the medium access and sampling rate in the rate adjustment by compressing data into variable sizes chunks. The mentioned works suffer from the high computing burden on the remote monitoring device comparing to event-based alternatives discussed previously.

The authors proposed an optimal state estimation framework for microgrids using the send-on-delta (SoD) sampling method, in their previous work [23]. The proposed SoD sampling method was delay independent, which only checked if the signal has crossed a predefined threshold as the main condition for the event transmission. Considering the scale of the IoT sensors installed across a microgrid, which can be of thousands or more, this method is an inefficient usage of the communication bandwidth. Also, in that work, the effect of the communication delay was not considered, which is important in IoT wireless sensor networks. Therefore, in this article to address the network limitations, computational complexity, and microgrid requirements, a novel solution is proposed that considers the effect of communication delay by adaptively adjusting the threshold of SoD sampler, based on the proposed event-based average consensus protocol. The proposed estimator employs projection onto convex sets (POCS) technique [24] to optimally reconstruct the sparse signals from the measurement nodes and reduces the state estimation error of event-based Kalman filter.

The contributions of this work can be summarized as the proposal of the following items:

- 1) An optimal event-based state estimation framework for microgrids that consists of the proposed event-triggered Kalman filter with the POCS-based signal reconstruction.
- 2) An adaptive threshold SoD sampling method to mitigate the communication delay for accurate state estimation.
- 3) An event-based average consensus protocol for average delay consensus of sampling units such as smart meters.

This article is organized as follows. In Section II, data modeling for both ac and dc microgrids and the architecture of the estimator are discussed. An overview of the observer design process is provided in Section III. Then after, the event-based Kalman filter is developed in Section IV and the POCS signal reconstruction technique is discussed in Section V. The time delay consensus protocol for adaptive threshold SoD sampling is provided in Section VI. The optimality of the solution is analyzed from different aspects in Section VII. In Section VIII, the results

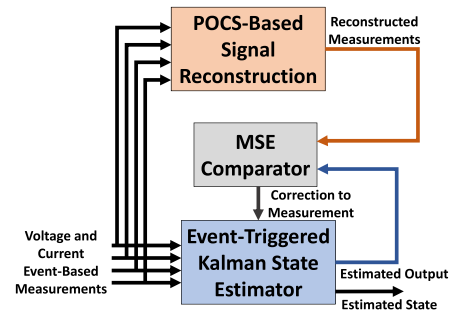


Fig. 1. Proposed event-based structure for microgrid state estimation.

for validation of the observer performance are provided, which is evaluated on an experimental dc microgrid test-bench. The model used for the closed loop control system is derived from our previous work in [1], in which we have proposed a distributed control system for dc microgrids. Finally, Section IX concludes this article.

II. MICROGRID STATE ESTIMATION DATA MODELING AND THE OBSERVER ARCHITECTURE

In this section, the microgrid state estimation problem is modeled from the measurement data viewpoint. A microgrid usually consists of energy storage (ES) systems, RESs, consumer loads, and power converters. Generally, two voltage systems are considered for microgrids: dc (direct current) and ac (alternating current) microgrids. Each of these different types are dynamic systems that can be modeled using a set of (non)linear differential equations. Like any other type of dynamical system, every process has internal state variables, outputs, and inputs. The measurements set for the ac and dc microgrids state estimation are {Active power injected into each bus, Reactive power injected into each bus, rms voltage of buses} and {rms voltage of buses, rms of the injected current into each bus}, respectively. Other variables such as phase can be considered for ac microgrids as well, but the phasor measurement units (PMUs) are required for this high speed synchronization, which can be expensive. Therefore, indirect measurements with active and reactive power are used here, which have higher feasibility with lower cost. It is assumed that the measurements from the distributed sensors have the following error dynamics:

$$\mathbf{z} = \mathbf{h}(x) + \begin{bmatrix} \mathbf{e}_1 \mathbf{e}_2 \dots \mathbf{e}_n \end{bmatrix}^T \quad (1)$$

where \mathbf{z} is the output of the sensors, $\mathbf{h}(x)$ is the state to output mapping, and \mathbf{e}_i is the sensor error, which can be due to the noise, or inaccuracy. Also the state dynamics are modeled with the nodal admittance matrix (\mathbf{Y} bus) of the grid.

The architecture of the proposed state estimator with event-based measurements is shown in Fig. 1. The three parts are: the event-based adaptive Kalman state estimator, the event-based signal reconstructor, and the mean square error (MSE) comparator. The microgrid estimation input quantities are collected using the proposed adaptive SoD measurement technique. The event-based Kalman filter works based on the knowledge that the signal between the events is bounded by the δ threshold

in the SoD sampler. The original signal is reconstructed in the signal conditioner based on the received events using the POCS algorithm, which is mainly used in the literature as a promising approach for low quality image reconstruction. In the last stage, the error comparator updates the estimated state input based on the difference between the reconstructed signal and the predicted output of the previous filtering stage. The SoD sampler threshold is adapted distributively based on the consensus value of the average communication delay. In this mechanism, each sensor calculates the round trip delay between itself and the microgrid estimator and adjusts the threshold according to the fused data from neighbor sensors. The main advantage of this mechanism shows itself when the microgrid components communicate over a shared wireless medium, which is usually the case in IoT-enabled microgrids [4]. Optimal usage of network resources, meanwhile providing a high quality estimate of the microgrid state is the aim of the proposed estimation strategy. For example, consider that a microgrid is operating in a transient mode. Usually, in transient modes, the system exposes fast dynamics that lead to a very large number of events using the delay-independent SoD sampling method, which was tackled in our previous work [4]. Communication delay directly proportional to the traffic rate (or packet generation rate) in a shared medium. As a result, the delay on the shared communication medium increases, which considerably decreases the quality of data, and the state estimation accuracy. However, in our proposal, if the sensors achieve a consensus on the average communication delay on the shared communication medium, they can automatically adjust the SoD sampling threshold to a wider region, which leads to a lower number of events generated. As a result of this adaptivity, the quality of the data and the state estimation accuracy will be improved considerably, comparing to the previous proposed delay-independent method. To provide this average delay consensus for the sensors in a microgrid, a novel event-based average consensus protocol is proposed in Section VI, which works in parallel with the SoD sampling data flow.

III. DESIGN PROCESS OF THE STATE ESTIMATOR

This section summarizes the steps required for the microgrid state estimator, in a simplified sequence:

- 1) Finding the global small signal model of the microgrid in the form of a linear state space equation. In this step, the covariance for the process noise and the measurement noise should be chosen according to the microgrid specifications and sensor accuracies. In this work, we have converted the closed loop transfer function matrix, defined in equation (36) of [1], into minimal state space model to get equation (2).
- 2) Choosing the initial value for the threshold of the SoD sampler. This value should be selected in accordance with the covariance values chosen in the previous steps, in order to prevent the noisy measurements to generate unnecessary events and the resulted traffic.
- 3) Building the communication topology graph for the event-based average consensus protocol defined in Theorem 1. The graph should be strongly connected, but

doesn't need to be deterministic, as the average consensus protocol, designed in the next step, adjusts the SoD threshold dynamically.

- 4) Choosing the average consensus parameters to have a guaranteed convergence rate for the consensus protocol. This value affects the event generation, therefore a trade-off takes place between the number of events and the convergence rate of the protocol.

After these steps are taken in the design process, the parameters of the state estimator and the nodes are initialized with the corresponding microgrid parameters. In the results section, the values for the parameters of the case study microgrid are provided together with the results of the experiment. In the next section, the mathematical framework of the event-based Kalman filter with SoD sampling is developed.

IV. EVENT-BASED KALMAN FILTER BASED ON SOD

Minimal realization of the microgrid admittance bus (Y bus) and the small signal model of the controllers, results in the following multivariable system for the estimation problem:

$$\begin{aligned}\dot{x} &= Ax(t) + w(t) \\ y(t) &= Cx(t) + v(t)\end{aligned}\quad (2)$$

where $x \in \mathbb{R}^n$ is the system state and $y \in \mathbb{R}^p$ is the measured output. $w(t)$ and $v(t)$ are the process noise and measurement noise, respectively, which are the uncorrelated, zero-mean white Gaussian random processes, satisfying the following:

$$E \{w(t) w(s)'\} = Q \delta(t - s) \quad (3)$$

$$E \{v(t) v(s)'\} = R \delta(t - s) \quad (4)$$

$$E \{w_i(t) v_j(s)'\} = 0, \quad 1 \leq i \leq n, \quad 1 \leq j \leq p. \quad (5)$$

R is the measurement noise covariance, and Q is the process noise covariance. Also, w_i and v_j are the i th and j th elements of the w and v , respectively. It is presumed that the i th sensor only transmits the data when the difference between the current value and the previous value is greater than the SoD threshold δ_i . Using SoD method [25], the estimator continuously samples the data with a period of T from the measurement nodes. For example, if the last received i th sensor value is y_i at time $t_{\text{last},i}$, and there is no data received from i th node for $t > t_{\text{last},i}$, then $y_i(t)$ is estimated as

$$y_i(t_{\text{last},i}) - \delta_i \leq y_i(t) \leq y_i(t_{\text{last},i}) + \delta_i. \quad (6)$$

The last received i th sensor data is used to compute the output $y_{\text{computed},i}$ even if there is no sensor data transmission:

$$y_{\text{computed},i}(t) = y_i(t_{\text{last},i}) = C_i x(t) + v_i(t) + \Delta_i(t, t_{\text{last},i}) \quad (7)$$

where $\Delta_i(t, t_{\text{last},i}) = y_i(t_{\text{last},i}) - y_i(t)$ and:

$$|\Delta_i(t, t_{\text{last},i})| \leq \delta_i. \quad (8)$$

In (7), measurement deviation increases from $v_i(t)$ to $v_i(t) + \Delta_i(t, t_{\text{last},i})$. $\Delta_i(t, t_{\text{last},i})$ is assumed to have the uniform distribution constrained by (8), therefore the variance of $\Delta_i(t, t_{\text{last},i})$ is $\frac{(2 \times \delta_i)^2}{12}$, which will be added to the *output noise covariance matrix*, $R(i, i)$, in the Kalman estimator.

SoD-based State Estimation Algorithm: In order to suitably improve the *update* part of the standard Kalman filter algorithm, an improved algorithm is proposed here, which makes it adapted to the SoD event triggering condition by increasing the input covariance \bar{R}_k , at the instant of the events

1) Initialization step

$$\begin{aligned} \hat{x}^-(0), P_0^- \\ y_{\text{last}} = C\hat{x}^-(0). \end{aligned} \quad (9)$$

2) Input measurement update

$$\bar{R}_k = R \quad (10)$$

if *i*th event are received

$$\hat{y}_{\text{last},i} = y_i(kT) \quad (11)$$

else

$$\bar{R}_k(i, i) = \bar{R}_k(i, i) + \frac{(2 \times \delta)_i^2}{12} \quad (12)$$

end if

$$\begin{aligned} K_k &= P_k^- C' (C P_k^- C' + \bar{R}_k)^{-1} \\ \hat{x}(kT) &= \hat{x}^-(kT) + K_k (\hat{y}_{\text{last}} - C\hat{x}^-(kT)) \\ P_k &= (I - K_k C) P_k^- \end{aligned} \quad (13)$$

3) Project ahead

$$\begin{aligned} \hat{x}^-((k+1)T) &= \exp(AT)\hat{x}(kT) \\ P_{k+1}^- &= \exp(AT)P_k \exp(A'T) + Q_d \end{aligned} \quad (14)$$

where Q_d is the covariance of the process noise for the discretized microgrid state space realization, and y_{last} is defined as follows (15):

$$y_{\text{last}} = [y_{\text{last},1}, y_{\text{last},2}, \dots, y_{\text{last},p}]'. \quad (15)$$

The presented event-based estimator is also able to be used in the implementation of the distributed controllers in networked systems. For further studies on the convergence analysis, one may refer to [7]. It should be noted that in the proposed event-based observer, convergence is achieved by knowing the fact that Kalman filter is an optimal observer. Nevertheless, choosing smaller values for δ_i would result in the a significant decrease in convergence time [25].

V. SIGNAL RECONSTRUCTION FORMULATION AND ESTIMATOR UPDATE RULE

The SoD sampled version of a signal contains the time instants that the original signal has changed more than the threshold in the SoD sampling (i.e., δ). If no sample has been generated by the SoD sampler, then it means that the original signal has remained in the region around the last event value with the radius of δ . Here, this is called the implicit information in the event data, which is used to solve the optimization problem of signal fitting and reconstruction. To formulate the optimization problem, the solution boundaries need to be determined. The implicit information from the SoD sampled signals are used to determine the required boundaries for the solution of the convex optimization problem, which is modeled in the following. To model and

solve the optimization problem, POCS technique is used, which has been previously used for image reconstruction from low resolution cameras [26], [27], and for signal recovery from level crossing samples [28]. SoD sampling is a generalization of level crossing or Lebesgue sampling, which also considers the signal initial value. To adjust this sampling technique to POCS formulation, the results of level-crossing sampling from [24] is extended, detailed in the next section.

A. Implicit Information of SoD Sampled Signal

SoD sampling is a type of event-based sampling, where each event shows a crossing of the signal $x(t)$ from a one dimensional region bounded by δ around the last sample. The event time instants $t_n \in \mathbb{Z}$, $n \in \mathbb{Z}$ are defined as:

$$t_n = \min\{t > t_{n-1}, x(t) - x(t_{n-1}) > \delta\}. \quad (16)$$

The output of SoD sampler is the sequence of pairs $(t_n, x(t_n))$. The set of possible samples by assuming zero initial conditions is $X_e = \{x(t_0), x(t_1), x(t_2), \dots, x(t_n)\}$. In order to formulate the convex optimization problem, a convex region for the possible range of the reconstructed signal is defined according to (16):

$$\theta^-(t) \leq x(t) < \theta^+(t) \quad (17)$$

where $\theta^-(t)$ and $\theta^+(t)$ are the piece-wise constant lower and upper boundaries, respectively, that are created from the following constraints:

$$\begin{aligned} \theta^-(t) &= \{r \in \mathbb{R}, r = x(k) - \delta, k \in t_n\} \\ \theta^+(t) &= \{r \in \mathbb{R}, r = x(k) + \delta, k \in t_n\}. \end{aligned} \quad (18)$$

With this definition, the sign of the signal slope at the event instants (t_n) is defined as

$$S(t_n) = \begin{cases} x(t_n) - x(t_{n-1}), & x(t_n) \neq x(t_{n-1}) \\ S(t_{n-1}), & x(t_n) = x(t_{n-1}) \end{cases}. \quad (19)$$

The samples along with the implicit boundary information, take a form of sets membership. Therefore the solution for the reconstructed signal $x(t)$ will fall into the following convex sets ($C(\mathbb{R})$ and \mathbb{L}^2 denote continuous function and Hilbert space, respectively):

- 1) From the explicit information (signal values at the time of events)

$$\xi = \{u(t) \in C(\mathbb{R}) : u(t_n) = x(t_n) \text{ for all } n \in \mathbb{Z}\}. \quad (20)$$

- 2) From the implicit information (the value of the threshold that generated this event)

$$\mathbb{I} = \{u(t) \in C(\mathbb{R}) : \theta^- \leq u(t) < \theta^+(t) \text{ for all } t \in \mathbb{R}\}. \quad (21)$$

- 3) From the knowledge that the signal is band-limited with maximum frequency Ω (Fourier decomposition of the highest order dynamics in the signals of the system)

$$\mathbb{B} = \left\{ u(t) \in \mathbb{L}^2(\mathbb{R}) : \forall |\omega| > \Omega, \int_{-\infty}^{+\infty} u(t) e^{-j\omega t} dt = 0 \right\}. \quad (22)$$

The set \mathbb{B} is convex as the band-limited signals form a linear space. For the sets \mathbb{I} and ξ , [24] provides the proof of convexity. The reconstructed signal should be a member of the set $\xi \cap \mathbb{I} \cap \mathbb{B}$ as the constraint of the optimization. This constraint is usually a large region that makes finding the optimal solution a computation intensive task. Fortunately, because $\theta^-(t) \leq x(t) < \theta^+(t)$, one can easily derive that $\mathbb{I} \subset \xi$. Therefore, the constraint is limited to the boundary defined by $\mathbb{I} \cap \mathbb{B}$, which needs less computations for the task of real-time signal estimation.

B. POCS Signal Reconstruction

There are two methods to solve the formulated POCS problem in the literature, one-step and iterative projection. A detailed comparison of these two methods is provided in [24]. As real-time state estimation for microgrids is the aim of this article, the later method of iterative POCS are used, which exhibits fast computations with low precision loss. Iterative solution for POCS works by having two or more convex sets, and on each iteration the initial solution is projected to one of those convex solutions sets. By repeating the projection iteratively to those sets, the initial estimate gets closer to the optimal solution.

The projection of the signal g onto a continuous convex set C results in another signal $\hat{x}(t)$, which is nearest to signal g

$$\hat{x} = P_{Cg} = \arg \min_{y \in C} \|g - y\| \quad (23)$$

where the projection P_{Cg} is closer to any $y \in C$ than g

$$\|P_{Cg} - x\| < \|g - y\|. \quad (24)$$

For the event-based signal reconstruction problem, the initial guess \hat{x}_0 should be first projected onto convex set \mathbb{B} with the following projection operator:

$$\begin{aligned} P_{\mathbb{B}g}(t) &= \hat{x}(t) * \frac{\Omega}{\pi} \text{sinc}(\Omega t) \\ &= \int_{-\infty}^{\infty} \hat{x}(\tau) \frac{\Omega}{\pi} \text{sinc}(\Omega(t - \tau)) d\tau \end{aligned} \quad (25)$$

having defined $\text{sinc}(y) = \frac{\sin(y)}{y}$. (* is the convolution)

The projection operator onto convex set \mathbb{I} for clipping the signal to the boundary defined by θ is

$$P_{\mathbb{I}g}(t) = \begin{cases} \theta^+(t), & \hat{x}(t) > \theta^+(t) \\ \hat{x}(t), & \theta^-(t) \leq \hat{x}(t) < \theta^+(t). \\ \theta^-(t), & \hat{x}(t) < \theta^-(t) \end{cases} \quad (26)$$

Finally, by applying this operator for both projections, the desired accuracy of signal reconstruction will be achieved

$$\hat{x}_{m+1} = P_{\mathbb{B}g} P_{\mathbb{I}g} \hat{x}_m, \quad m \in \mathbb{Z}. \quad (27)$$

The condition for stopping the projections depends on the required accuracy measures and is application dependant. By practical experiments, authors have found that 10 iterations provides an acceptable accuracy for the microgrid experiment duration, which is used in the experiment.

C. MSE Comparator Update Rule

Normally, the measurements from the nodes arrive with the added noise signal. The noise is assumed to be the derivative of the Brownian motion, which is called white noise or Gaussian noise. The traditional Kalman filter is built on top of this assumption that the noise is Gaussian, however, by using the SoD sampling technique, the reconstructed signal becomes a non-Gaussian stochastic process. This leads to degradation of the estimation accuracy and longer convergence time, if it converges. Therefore, an estimator update rule is proposed here that compares the output of the Kalman filter and the reconstructed signal in real-time, and injects the correction value to the input of the Kalman filter, respectively. The correction is a dynamic offset value, which is added as described in the following:

$$y_i(t_{\text{last},i}) = \begin{cases} y_i(kT), & \|y_{i_{\text{predict}}} - y_{i_{\text{construct}}}\| < \delta \\ y_{i_{\text{construct}}}(kT), & \|y_{i_{\text{predict}}} - y_{i_{\text{construct}}}\| \geq \delta \end{cases} \quad (28)$$

where $y_{i_{\text{predict}}}$ and $y_{i_{\text{construct}}}$ are the output of the signal reconstructor and the event-based Kalman filter, respectively.

VI. EVENT-BASED AVERAGE DELAY CONSENSUS

Each measurement unit, calculates the estimator communication link delay using acknowledgment round-trip delay (RTD) [29]. This value is then shared with neighbor units using the proposed event-based communication protocol. Each unit then decides the value of its SoD sampler threshold based on the average communication delay, using a linear droop mapping. In other words, when the average delay increases, the threshold for SoD sampling is also increased in order to reduce the network traffic. The droop rate can be different for the units, which provides the potential to prioritize the sampling of each unit, however, for simplicity of the , a shared practical droop value is assumed in this article. The value of the droop is tuned based on the IoT network setup of the microgrid. In the following section, the event-based average delay consensus protocol is described.

A. Basic Graph Theory

The measurement unit are connected by an undirected graph $\mathcal{G}(\mathcal{V}, \mathcal{E})$ with the nodes or vertices $\mathcal{V} = (1, \dots, N)$, and the set of edges $\mathcal{E} \subset \mathcal{V} \times \mathcal{V}$. The nodes in the graph represent the measurement units, and the edges denoting the communication link between the nodes. The condition $(i, j) \in \mathcal{E}$ holds if there is a link allowing the information flow from node i to node j and vice versa. $A = [a_{ij}] \in \mathbb{R}^{N \times N}$, represents the graph adjacency matrix, where $a_{ij} > 0$ if $(i, j) \in \mathcal{E}$, and $a_{ij} = 0$ otherwise. $d_i = \sum_{j=1}^N a_{ij}$ denotes the weighted degree of agent v_i . The degree matrix of the graph is given by $\mathbf{D} = \text{diag}\{d_i\}$, and the Laplacian matrix of the graph is derived from $\mathbf{L} = \mathbf{D} - \mathbf{A}$. An undirected graph is connected, if there exists at least one path between any two agents.

B. Average Consensus Protocol

By considering a multiagent network with N single integrator agents, the distributed average consensus will be

$$\dot{x}_i = u_i(t) = - \sum_{j=1}^N L_{ij} x_j(t). \quad (29)$$

Since it is often not practical to have a continuous stream of data over a communication link, it is considered that each agent broadcasts its state information at specific instances (i.e., event instances) to its neighbors. Hence, we propose the following event-triggered consensus protocol:

$$\dot{x}_i = u_i(t) = - \sum_{j=1}^N L_{ij} \hat{x}_j(t). \quad (30)$$

The increasing sequence $\{t_l^i\}_{l=1}^{\infty}$ and $\{t_{l+1}^i - t_l^i\}_{l=1}^{\infty}$, are called the triggering times and inter-event times of agent i , respectively. In order to simplify the notations, let $x(t) = [x_1(t), \dots, x_n(t)]^T$, $\hat{x}(t) = [\hat{x}_1(t), \dots, \hat{x}_n(t)]^T$, and $e(t) = [e_1(t), \dots, e_n(t)]^T = \hat{x}(t) - x(t)$. The aim is to find the correct event-triggering condition to prove the stability of the proposed consensus protocol. We state the following theorem, knowing the fact that λ_2 is the second smallest eigenvalue of L , using Lemma 1.

Lemma 1. [30]: The Laplacian matrix L of a connected graph \mathbb{G} is positive semidefinite, i.e., $z^T L z \geq 0, \forall z \in \mathbb{R}^n$. Moreover, $z^T L z = 0$ if and only if $z = a \mathbf{1}_n, a \in \mathbb{R}$, and $0 \leq \lambda_2(L) K_n \leq L$, where λ_2 is the second smallest eigenvalue of L and $K_n = I_n - \frac{1}{n} \mathbf{1}_n \mathbf{1}_n^T$.

Theorem 1: Consider a strongly connected multiagent directional graph with N agents and the consensus protocol defined in (30). Let $0 < \sigma_i < 1$ be a constant design parameter. Given the first triggering time $t_1^i = 0$, the network exponentially achieves average consensus under the event-triggering function given as follows:

$$e_i^2(t) - \frac{\sigma_i}{4L_{ii}} \sum_{j=1}^N L_{ij} (\hat{x}_j(t) - \hat{x}_i(t))^2 \leq 0 \quad (31)$$

with the convergence rate, upper bounded by

$$\exp\left(-\frac{(1 - \sigma_{\max}) \min_i \{L_{ii}\} \lambda_2(L) t}{2 \min_i \{L_{ii}\} + \|L\| \sigma_{\max}}\right). \quad (32)$$

Proof: Following the notation of [31], $\delta(t)$ is defined as the disagreement vector with the following change of variable:

$$x(t) = a \mathbf{1} + \delta(t) \quad (33)$$

where a is average of the initial state values, $a = \frac{1}{N} \sum x_i(t)$. Using (33), the control input of the agents will be derived as

$$\begin{aligned} \dot{\delta}(t) &= - \sum_{i=1}^N L_{ij} (a + \hat{\delta}_j(t)) \\ &= -a \sum_{i=1}^N L_{ij} - \sum_{i=1}^N L_{ij} \hat{\delta}_j(t) \\ &= - \sum_{i=1}^N L_{ij} \hat{\delta}_j(t). \end{aligned} \quad (34)$$

Now to prove the stability, we propose the following Lyapunov function, which covers the dynamics of consensus:

$$V(\delta(t)) = \frac{1}{2} \sum_{i=1}^N \delta_i^2 \geq 0. \quad (35)$$

The derivative of the Lyapunov function along the dynamic trajectory (30) will be

$$\begin{aligned} \dot{V}(\delta(t)) &= \sum_{i=1}^N \delta_i \dot{\delta}_i = \sum_{i=1}^N \delta_i \sum_{j=1}^N -L_{ij} \hat{\delta}_j(t) \\ &= \sum_{i=1}^N (\hat{\delta}_i - e_i(t)) \sum_{i=1}^N -L_{ij} \hat{\delta}_j(t) \\ &= \frac{1}{2} \sum_{i=1}^N \sum_{j=1}^N L_{ij} (\hat{\delta}_j(t) - \hat{\delta}_i(t))^2 \\ &\quad - \sum_{i=1}^N \sum_{j=1}^N e_i(t) L_{ij} \hat{\delta}_j(t) \\ &= \frac{1}{2} \sum_{i=1}^N \sum_{i=1}^N L_{ij} (\hat{\delta}_j(t) - \hat{\delta}_i(t))^2 \\ &\quad - \sum_{i=1}^N \sum_{j=1, j \neq i}^N e_i(t) L_{ij} (\hat{\delta}_j(t) - \hat{\delta}_i(t)). \end{aligned} \quad (36)$$

To simplify (36), let

$$\hat{f}_i = - \sum_{i=1}^N L_{ij} (\hat{\delta}_j(t - \tau_{ij}) - \hat{\delta}_i(t))^2. \quad (37)$$

Therefore (36) becomes

$$\dot{V}(\delta(t)) = \frac{1}{2} \sum_{i=1}^N \hat{f}_i - \sum_{i=1}^N \sum_{j=1, j \neq i}^N e_i(t) L_{ij} \hat{\delta}_j(t). \quad (38)$$

Since $ab < a^2 + \frac{1}{4}b^2, \forall a, b \in \mathbb{R}$, and

$$\sum_{i=1}^N \hat{f}_i = - \sum_{i=1}^N \sum_{j=1}^N L_{ij} (\hat{\delta}_j(t - \tau_{ij}) - \hat{\delta}_i(t))^2 = \hat{\delta}^T(t) L \hat{\delta}(t) \quad (39)$$

the following inequality holds

$$\begin{aligned} \dot{V}(\delta(t)) &\leq -\frac{1}{2} \sum_{i=1}^N \hat{f}_i - \sum_{i=1}^N \sum_{j=1, j \neq i}^N L_{ij} e_i^2(t) \\ &\quad - \sum_{i=1}^N \sum_{j=1, j \neq i}^N L_{ij} \frac{1}{4} (\hat{\delta}_j(t - \tau_{ij}) - \hat{\delta}_i(t))^2 \\ &= -\frac{1}{4} \sum_{i=1}^N \hat{f}_i + \sum_{i=1}^N L_{ij} e_i^2(t). \end{aligned} \quad (40)$$

From (31) and (40), we have

$$\begin{aligned} \dot{V}(\delta(t)) &\leq -\frac{1}{4} \sum_{i=1}^N \hat{f}_i + \sum_{i=1}^N L_{ij} e_i^2(t) \\ &\leq -\frac{1}{2} (1 - \sigma_{\max}) \hat{\delta}^T(t) L \hat{\delta}(t). \end{aligned} \quad (41)$$

where $\sigma_{\max} = \max\{\sigma_1, \dots, \sigma_n\}$. In addition, we have

$$\begin{aligned} \delta^T(t)L\delta(t) &= (\hat{\delta}(t) + e(t))^T L(\hat{\delta}(t) + e(t)) \\ &\leq 2\hat{\delta}^T(t)L\hat{\delta} + 2e^T(t)L e(t) \end{aligned} \quad (42)$$

$$\leq 2\hat{\delta}^T(t)L\hat{\delta} + \frac{\|L\|\sigma_{\max}}{2\min_i\{L_{ii}\}} \sum_{i=1}^N \hat{f}_i \quad (43)$$

$$= \left(2 + \frac{\|L\|\sigma_{\max}}{2\min_i\{L_{ii}\}}\right) \hat{\delta}^T(t)L\hat{\delta} \quad (44)$$

where (42) holds because L is a positive semidefinite matrix and $2a^T L b \leq a^T L a + b^T L b, \forall a, b \in \mathbb{R}^n$ and (43) holds since (31) and $a^T L a \leq \|L\| \|a\|^2, \forall a \in \mathbb{R}^n$. Finally we have

$$\begin{aligned} \dot{V}(\delta(t)) &\leq -\frac{(1 - \sigma_{\max})\min_i\{L_{ii}\}}{4\min_i\{L_{ii}\} + 2\|L\|\sigma_{\max}} \delta^T(t)L\delta(t) \\ &\leq -\frac{(1 - \sigma_{\max})\min_i\{L_{ii}\}\lambda_2(L)}{2\min_i\{L_{ii}\} + 1\|L\|\sigma_{\max}} V(\delta(t)) \end{aligned} \quad (45)$$

(45) holds due to Lemma 1, hence

$$\dot{V}(\delta(t)) \leq V(\delta(0)) \exp\left(-\frac{(1 - \sigma_{\max})\min_i\{L_{ii}\}\lambda_2(L)t}{2\min_i\{L_{ii}\} + \|L\|\sigma_{\max}}\right). \quad (46)$$

This shows that the multiagent system (30) with event-triggering condition (31) exponentially reaches stability, as long as \mathcal{G} is connected. ■

VII. ANALYSIS OF THE OBSERVER OPTIMALITY

The optimality of the proposed solution can be analyzed from several aspects. From the state estimation aspect, the employed Kalman state estimator is known to be an optimal linear state estimator in the literature of state estimation. It follows from theory that the Kalman filter is the optimal linear filter in cases where

- 1) The model perfectly matches the real system.
- 2) The measurement noise is white (uncorrelated).
- 3) The covariances of the noise are exactly known.

When a Kalman filter works optimally, the update sequence (the output prediction error) is white noise, therefore the whiteness property of the updates defines the estimation performance. The existence, optimality and stability of the Kalman filter with partial observations are discussed in [32].

The proposed POCS signal re-Constructor is a recursive method that converges to a convex set consisting of the original signal after several iterations. The reconstructed signal found by the POCS method, is an optimal solution that can be build from the SoD generated samples. The convergence to the solution is proved in [33] along with the analysis on the convergence rate. From the communication and channel utilization aspect, the solution is optimal compared to the traditional time-based sampling technique such as zero-order-hold. In the proposed solution, the network packet is only generated when there is a deviation from the SoD threshold or the average consensus protocol requires a new data-sharing event.

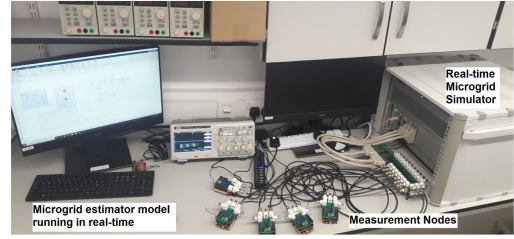


Fig. 2. Experimental setup for evaluation of the proposed estimator.

VIII. ESTIMATOR VALIDATION RESULTS

In order to evaluate the state estimator performance, an IoT-based setup is designed that consists of IoT smart meters based on Seeeduno Dragon IoT evaluation boards and a dc microgrid real-time simulator from dSPACE (SCALEXIO Real-Time Simulator). Each node has a long range wide area network (LoRaWAN) communication module and supports IEEE 802.11 b/g/n (WiFi) communication protocol. The nodes are interfaced to the real-time microgrid simulator via an interface stackable shield that can measure analog input and output signals. The setup is shown in Fig. 2. The proposed SoD sampling strategy is implemented using digital signal processing instructions of ARM Cortex M0+, and the microgrid model is implemented by using MATLAB/Simulink real-time code generator. WiFi protocol necessitates a router gateway to be used for the data collection. In this setup, a Raspberry Pi computer with the supporting communication modules for the gateway operation is used. This gateway receives the data from the measurement nodes via MQTT (Message Queuing Telemetry Transport) protocol. Thingsboard software implements the MQTT broker, which is used for data archiving and processing. By using the mentioned protocols and devices, the microgrid monitoring cost can be considerably cheaper than other smart metering technologies such as IEC 61850 [34]. The state estimator was implemented on the real-time microgrid simulator. The nodes measure the signals and transmit them over the wireless network to the real-time simulator. Therefore, all of the results are observed at the real-time simulator. The IEEE 5 bus reference microgrid with the nominal 110 V bus voltage and 10 kW reference power for per-unit calculations, as shown in Fig. 3, is chosen for the case study. The droop controllers are designed based on the technique proposed in [1]. The Y bus admittance matrix for state representation of the microgrid is derived based on the line parameters in Table I. Also the covariance parameters and initial SoD threshold of the estimator is shown in Table II. The IEEE 5 bus microgrid system is standardized with a set of reference line parameters which includes the resistance, reactance, and the susceptance of the lines based on 50 Hz ac frequency. In a dc microgrid, the values of resistance, inductance, and capacitance are the important line dynamics required to be modeled in the simulation. Therefore, we have converted the corresponding values in the ac system to their equivalent dc system with the following simple formula in per-unit: $R_{dc} = R_{ac}$ (not considering the corona effect), $L_{dc} = \frac{X_L}{2*\pi*f}$, and $C_{dc} = \frac{2*\pi*f}{X_C}$

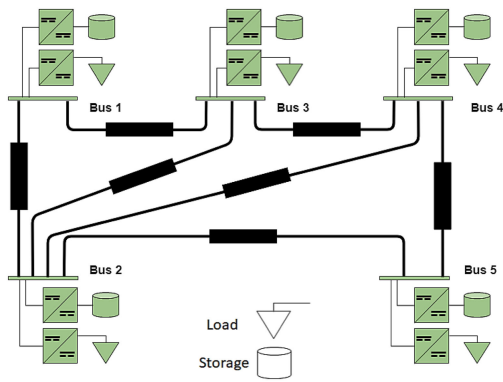


Fig. 3. IEEE 5 bus case study for estimator validation.

TABLE I
LINE PARAMETERS OF THE IEEE 5 BUS MICROGRID

Line	Line Impedance (p.u.)	Line Susceptance (p.u)
1-2	$0.02 + j0.06$	$j0.03$
1-3	$0.08 + j0.24$	$j0.025$
2-3	$0.06 + j0.25$	$j0.02$
2-4	$0.06 + j0.18$	$j0.02$
2-5	$0.04 + j0.12$	$j0.015$
3-4	$0.01 + j0.03$	$j0.01$
4-5	$0.08 + j0.24$	$j0.025$

TABLE II
STATE ESTIMATOR PARAMETERS FOR SIMULATION

$\delta(0)$ (threshold initial value)	1
Q (Process Noise Covariance)	0.1
R (Measurement Noise Covariance)	0.36
T (Estimator Sampling Time)	100 microseconds
σ_{max} (Even generation parameter)	0.6

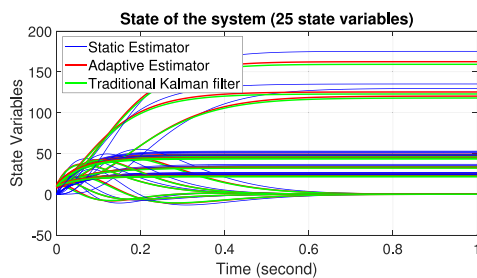


Fig. 4. Experiment result 1: State variables of the microgrid. The microgrid is realized into 25 state variables that need to be estimated by the proposed observer.

The simulations is run for 5 s, and the estimator converges to the actual state in 600 ms, as shown in Fig. 4. Furthermore, Fig. 5 shows that the proposed estimation strategy has achieved a better performance comparing to the traditional Kalman filter by converging to lower steady state error. For this simulation, the traditional Kalman filter runs in a digital platform with 0.1 ms period, needs 10000 events in 1 s to achieve the same

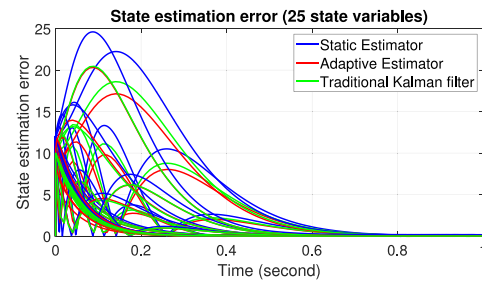


Fig. 5. Experiment result 2: The estimation error of the observers for comparison. The static estimator has a constant threshold with the value "1," and the adaptive estimator is initialized with the same value.

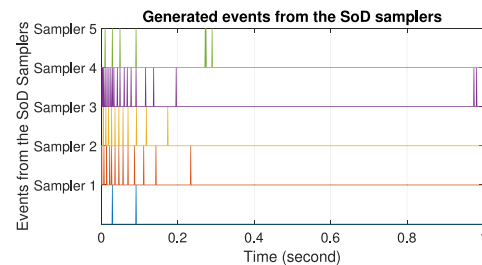


Fig. 6. Experiment result 3: Event generation density from the adaptive SoD sampler nodes. As can be seen, the number of generated events gets decreased as the system enters into its steady state mode.

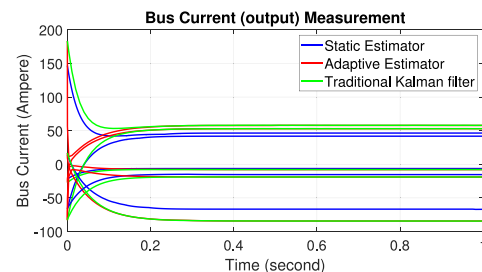


Fig. 7. Experiment result 4: The injected currents of the buses (system outputs). The nominal voltage is 110 V. Negative current means power generation and positive current means consumption at the buses.

performance as our proposed estimation strategy, with only a few hundred events. The Kalman filter has always been challenged for its high speed measurement requirements, however, the proposed estimator has opened new doors for event-based state estimators with low communication speed requirements. The event generation density over the time is shown in Fig. 6. Also as shown in Fig. 8, the steady state estimation error is comparatively lower comparing to the classic Kalman filter. The comparison of the observer methods are provided in Table III. From the network traffic perspective, Fig. 9 illustrates the comparison of the proposed adaptive SoD sampler estimator with the static threshold state estimator. The accumulative number of packets transmitted in the network, is reduced more than 40% from the static threshold SoD sampling method. Also, the existence of the threshold, guarantees that the Zeno behaviour will never happen, as can be seen in Fig. 6. During the experimental, it was found that the

TABLE III
COMPARISON OF THE OBSERVERS BY THEIR REQUIRED NETWORK CHARACTERISTICS

Observer	Sampling Type	Communication Delay	Resource Usage	Operation Type	Accuracy
Traditional (Classic) Kalman Filter [32]	Periodic	Not considered	High	Centralized	High
Static Threshold SoD-Based Kalman Filter [23]	Event-based	Not considered	Low	Centralized	Medium
Proposed Adaptive Observer with POCS Conditioner	Event-based	Adaptive	Medium	Distributed	High

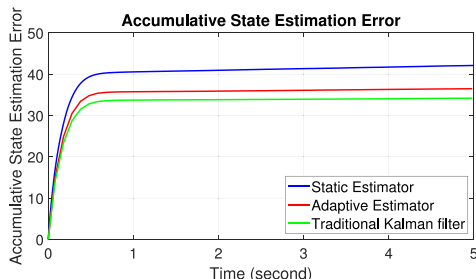


Fig. 8. Experiment result 5: Accumulative estimation error comparison between the traditional Kalman filter, the proposed adaptive threshold state estimator, and the static state estimator.

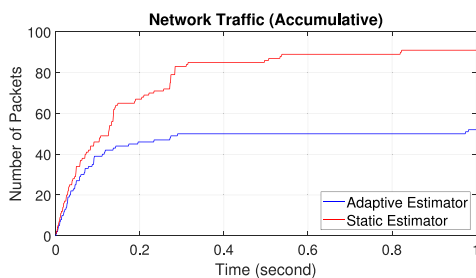


Fig. 9. Experiment result 6: Network traffic comparison between the static SoD sampler and the proposed adaptive strategy. It can be seen that the overall traffic is reduced by more than 40%.

LoRaWAN communication protocol has significant limitations, which can decrease the accuracy of estimation. It introduces a large value of delay between the events transmission in the range of seconds, especially when the number of messages per unit of time gets higher than the capacity of the network. The threshold of the SoD sampler directly affects the amount of messages, therefore a tuning algorithm will be required in order to make a relation between the estimation error, sampling threshold, and the number of events. Nevertheless, by using a high speed WiFi communication network, the ideal performance was achieved, fulfilling the data collection strategy requirements.

IX. CONCLUSION

In this article, an event-based optimal observer was proposed for the microgrids. The proposed estimator works based on SoD nonuniform sampling method and furthermore, the SoD threshold is adaptive with regard to the average communication delay. The average delay was decided using the event-based average consensus protocol. The estimation error was further corrected by POCS algorithm to have a higher estimation accuracy. It was resulted that the estimator has low estimation error comparing

to the classic Kalman filter, with only a few events exchanged in the communication network. The optimality of the solution was analyzed along with a step by step design procedure. The performance of the observer was studied in the reference IEEE 5 Bus microgrid. For the future study, the results can be extended to consider the packet drop out in the observer performance.

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